

Comparative Evaluation Of Effect Of Two Different Die Spacer Thickness On Internal Fit Of Metal Copings Fabricated By Computer-Aided Milling And Direct Metal Laser Sintering Techniques-An In-Vitro Study

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ABSTRACT

Background- Conventional technique to fabricate fixed partial framework is lost wax techniques. In this technique fabrication of the wax pattern is a critical step. It is time consuming task and dependent upon the skills of the dental laboratory technician. So this has subsequently evolved into CAD CAM Techniques. There are several laboratory studies that provide data on effect of fabrication technique on marginal and internal fit but limited data is available on effect of different die spacer thickness on internal fit of metal coping fabricated by CAD CAM techniques.

Aim - To evaluate and compare internal fit of metal copings fabricated by Milling and Direct Metal Laser Sintering Techniques with two different die spacer thickness.

Materials and Methodology - Full stainless steel die was machined milled. The Digital impression of the standardized master die was made using MEDITT310 lab scanner followed by generation of STL file for the master die using COLLAB20172.0.0.4 software. The STL file of the master die was used to generate STL file of the CAD Milled coping. The thickness of the coping was set to 0.5 mm. A spacer thickness was set to 40 μ m for 24 copings and to 65 μ m for 24 copings respectively. Milling was performed using ZUBLER DC5 milling machine. The generated STL file of master die was used for generating the STL file of the DMLS coping using 3M Designing software version 7 for DMLS. A spacer thickness of 40 microns was used as a virtual die spacer for 24 copings and 65 microns for 24 copings. Total sample size was 96. The measurement of three dimensional internal fit of CoCr copings were performed using a Triple Scan Protocol developed by Holst.

Results- Mean internal gap value for Subgroup A1 was 25.917 μ m with 5.7959 μ m as standard deviation and for Subgroup A2 it was found to be 29.519 μ m with 5.9908 μ m as standard deviation. Mean internal gap value for Subgroup B1 was 23.116 μ m with standard deviation of 2.7302 μ m whereas for Subgroup B2 it was found to be 21.264 μ m with standard deviation of 0.8954 μ m. Mean Internal gap values observed in Milling technique was statistically nonsignificant whereas, mean internal gap values observed in DMLS techniques showed statistically significant difference with 40 and 65 μ m die spacer thickness following an order of B2 < B1.

Conclusion

- In the current study, DMLS technique in comparison with Milled techniques showed lowest internal fit discrepancy for both 40 and 65 μ m die spacer thickness. However, within the DMLS technique, 65 μ m die spacer thickness showed least internal fit discrepancy followed by 40 μ m die spacer thickness.

Keywords- CAD CAM, DMLS, Milling, Co Cr coping, Internal fit, Die spacer thickness

I. INTRODUCTION

The fixed partial denture (FPD) is a common treatment available for the restoration of partially edentulous ridges, as it serves as excellent means of replacing missing teeth, where the dental implant is contraindicated.¹ Conventional technique to fabricate fixed partial framework is lost-wax technique. The possible problems with this technique are making impressions in the oral cavity which may cause discomfort for patients and inaccurate fit may result from dimensional change of impression material, distortion of wax patterns or irregularities in the cast metal.² The adoption of automated systems has in turn facilitated the development of a diverse range of fabrication methods, including the computer-aided subtractive technique milling and additive techniques such as Rapid manufacturing, Rapid prototyping, Stereo-lithography, Direct Metal Laser Sintering.^{3,4} The advantages of CAD/CAM techniques are simplicity, reduced costs and manufacturing time.^{5,6} Co-Cr based alloys are almost exclusively used for the production of metallic frameworks of RPDs and for the production of PFM prosthesis.⁷ Conventionally casted Co-Cr alloy based prostheses are difficult to fabricate due to high melting ranges and low laboratory usability. These inconveniences can be overcome by computer-aided design/computer-aided manufacturing (CAD/CAM) technique in which metal blocks are manufactured directly.⁸

Die spacing is a commonly used technique to provide space for the luting agent during cementation of prosthesis.⁹ Computer-aided design (CAD) technology provides the ability to virtually program the die spacer thickness.¹⁰ Success of fixed restorations depends on the ability of cemented restoration to resist dislodgement from tooth preparation. The interaction of 3 primary factors influence the potential for dislodgement: (1) Design of the tooth preparation, (2) Fit of the casting and (3) Nature of the cement. Close internal fit is one of the most important factors affecting the accuracy and the long-term success of the fixed prostheses.¹¹ Iwai et al. concluded that zirconia copings with cement spaces set to 60 μm showed better marginal and internal fit than copings with cement spaces set to 10 μm and 30 μm while Yildirim et al. found clinically acceptable margin and internal adaptation values for polymer infiltrated ceramic network material crowns using spacer setting of 40 μm.¹²

There are some laboratory studies that provide data on internal fit of metal copings fabricated by different CAD CAM techniques, limited data is available on effect of different die spacer thickness on internal fit of metal copings fabricated by different CAD CAM techniques. Thus aim of this study was to compare effect of two different die spacer thickness on internal fit of metal copings fabricated by Computer-Aided Milling and Direct Metal Laser Sintering techniques considering a null hypothesis that 'There is no difference in the internal fit of metal copings with different die spacer thickness fabricated by Computer-Aided Milling and Direct Metal Laser Sintering Techniques'.

II. MATERIALS AND METHODOLOGY

This study was planned to compare the effect of two different die spacer thickness (40 and 65 micrometer) on internal fit of metal copings fabricated by Subtractive technique (Computer-Aided Milling) and Additive technique (Direct Metal Laser Sintering).

Study Duration- 4 December 2020 to January 2022

Sample size - 96

Sample size calculation - Total of 96 samples of Co-Cr copings were fabricated which included 48 samples for each group and 24 samples for each subgroup (Fig 5).

$$\text{Sample size was calculated using the formula as } n = 2(Z\alpha + Z\beta)^2 \left[\frac{s}{d} \right]^2$$

where $Z\alpha$ is the z variate of alpha error i.e. a constant with value 1.96, $Z\beta$ is the z variate of beta error i.e. a constant with value. All samples were prepared from the Stainless steel Master die which was machined milled.

1 Group A – Copings fabricated by Milling technique (48 samples)

Subgroup A1 – Copings with 40 micrometer die spacer thickness (24 samples)

Subgroup A2 – Copings with 65 micrometer die spacer thickness (24 samples)

2 Group B – Copings fabricated by DML Stechnique (48 samples)

Subgroup B1 – Copings with 40 micrometer die spacer thickness (24 samples)

Subgroup B2 – Copings with 65 micrometer die spacer thickness (24 samples)

Total sample size - 96

Procedure methodology-

1 Fabrication of Master Die:

Full stainless steel die was machined milled (Fig 1) according to Shaikh SA et al (2014) with specific dimensions which were as follows¹³:

Length of die: 26.19 mm, Diameter at base: 12.70 mm, Crown height: 9.27mm, Diameter of crown: 9.22mm, Width of shoulder margin: 1.74mm, Angle of convergence: 2½ degree per wall.

2 Digital impression of the Master Die:

The Digital impression of the standardized master die was made using MEDITT310 lab scanner (Fig 2). The MEDITT310 series Scanner has a scan accuracy of 9 microns: ISO 12836 and ANSI/ADA specification no. 132, VDI-2634. The scanning of the die was performed followed by generation of STL files for the master die using COLLAB 20172.0.0.4 software.¹⁴

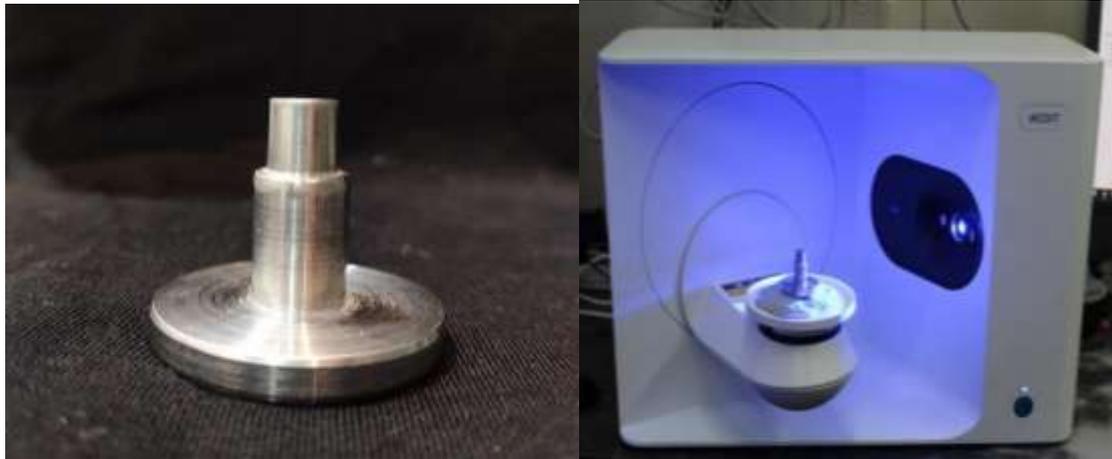


Fig1:Stainless Steel Master Die Fig2:Scanning of master die with Medit T310 lab scanner

3 Fabrication of CoCr Milled Copings (Group A):

The STL file of the master die was used to generate STL file of the CAD Milled coping. The generated STL file of the coping was used to mill non-presintered soft CoCr blocks (Ceramill sintron blanks; Amann Girrbach, Germany) to obtain CoCr copings by using software (Exocad V2.2, exocad GmbH, Darmstadt, Germany). The thickness of the coping was set to 0.5 mm. The spacer thickness was set to 40 µm for 24 copings and to 65 µm for 24 copings. Milling was performed using ZUBLER DC5 milling machine (Fig 3) which is a 5-axis milling machine.



Fig 3: ZUBLER DC5 Milling Machine



Fig 4: Direct Metal Laser Sintering EOS Germany Machine

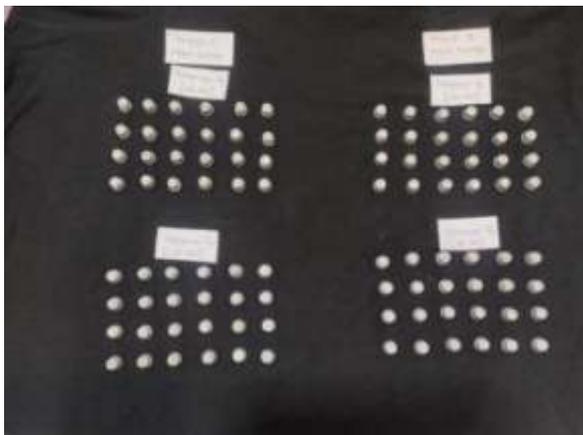


Fig 5: Co Cr Copings by Milling and DMLS



Fig 6: Scanning of Co-Cr Copings Techniques

4 Fabrication of Co Cr DMLS Copings (Group B) :

The generated STL file of master die was used for generating the STL file of the coping using 3M Designing software version 7 for DMLS. A spacer thickness of 40 microns was used as a virtual die spacer for 24 copings and 65 microns for 24 copings. The STL files, thus generated were used to obtain DMLS copings by Direct Metal Laser Sintering System EOS GERMANY (Fig 4). Thus total 48 Co Cr copings were obtained by DMLS technique.

5 Measurement of Three-Dimensional Internal Fit of Co Cr Copings:

The measurement of three dimensional internal fit of Co Cr copings was performed using a Triple Scan Protocol developed by Holst.¹⁵

This Process of obtaining data involved: 1) Scanning of Master Die (Fig 2) 2) Scanning of the Co Cr Coping (Fig 6) 3) Scanning of the Co Cr Coping placed on the master die in a clinically correct position. The scan of the master die and Co Cr Coping obtained in the study for fit assessment were superimposed with a common origin point.

The scan of the Co-Cr coping over the master die and the scan of master die were digitally superimposed using multiple reference points for performing best fit alignment. Following that, the scan of the Co-Cr coping and Co-Cr coping over the die were digitally superimposed. The scan of Co-Cr coping over the die was digitally subtracted to thus get the superimposition of the scan Co-Cr coping over the scan master die in best

possible alignment to provide the internal gap incut sections for Milled and DMLS Co-Cr copings.

Since it is a three dimensional internal fit evaluation multiple values were obtained at different points (buccopalatal section was divided into 3 subsections buccal, occlusal, palatal and mesiodistal section was divided into 5 subsections mesial, mesio-occlusal, occlusal, disto-occlusal and distal) and mean of those values was considered as internal fit discrepancy for that particular sample. The software used for assessment of the discrepancy was EXOCAD 2.3 MATERA software which helped in the superimposition and provided for discrepancies in cut sections between the Co-Cr coping and the master die.¹⁵

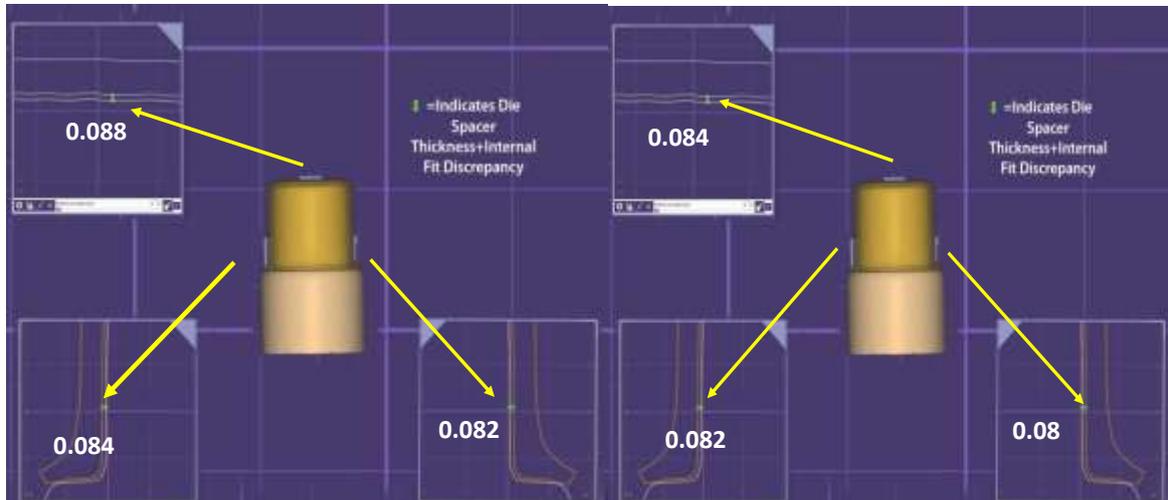


Fig 7: Cut Section of Internal Fit analysis for Milled Co Cr copings with 65 µm die spacer thickness

Fig 8: Cut Section of Internal Fit analysis for DMLS Co Cr copings with 65 µm die spacer

Statistical analysis

Data obtained was compiled on a MS Office Excel Sheet (v2019, Microsoft Redmond Campus, Redmond, Washington, United States). Data was subjected to statistical analysis using Statistical package for social sciences (SPSS v26.0, IBM). Descriptive statistics like Mean & SD, Median for numerical data has been depicted. Normality of numerical data was checked using Shapiro-Wilk test & was found that the data did not follow a normal curve; hence **non-parametric tests** were used for comparisons.

III. RESULTS

The mean internal gap value for Subgroup **A1** (Milled copings with 40 µm die spacer thickness) was **25.917 µm** with **5.7959 µm** as standard deviation and for Subgroup **A2** (Milled copings with 65 µm die spacer thickness) it was found to be **29.519 µm** with **5.9908 µm** as standard deviation (Table 1). The values suggest that there is a statistically highly significant difference with higher values in Subgroup A2 as compared to Subgroup A1, suggesting that the Internal gap values are higher for Milled metal copings with 65 µm die spacer thickness when compared with Milled metal copings with 40 µm die spacer thickness.

Mean internal gap value for Subgroup **B1** (DMLS copings with 40 µm die spacer thickness) was **23.116 µm** with standard deviation of **2.7302 µm** whereas for Subgroup **B2** (DMLS copings with 65 µm die spacer thickness) it was found to be **21.264 µm** with standard deviation of **0.8954 µm** (Table 1). These values suggest that there were higher values in Subgroup B1 as compared to Subgroup B2, suggesting that the internal gap values are higher for metal coping fabricated by DMLS technique with 40 µm die spacer thickness when compared with metal coping fabricated by DMLS technique with 65 µm die spacer thickness.

	Mean	Standard deviation	Standard error mean	Chi Square value	P value of Kruskal-Wallis Test
Subgroup A1	25.917	5.7959	1.1831	43.651	0.000**
Subgroup A2	29.519	5.9908	1.2229		
Subgroup B1	23.116	2.7302	0.5573		
Subgroup B2	21.264	0.8954	0.1828		

Table 1: Inter-Subgroup comparison of internal gaps between metal copings fabricated by Milling and DMLS techniques with 40 µm and 65 µm die spacer thickness (Kruskal-Wallis Test)

Mean internal gap value for Subgroup A1 (Milled copings with 40 µm die spacer thickness) was **25.917 µm** with standard deviation of **5.7959 µm** whereas for Subgroup B1 (DMLS copings with 40 µm die spacer thickness) it was found to be **23.116 µm** with standard deviation of **2.7302 µm** (Table 1). These values suggest that there is a statistically highly significant difference with high values in Subgroup A1 as compared to Subgroup B1, suggesting that the internal gap values for metal copings with 40 µm die spacer thickness were higher with copings fabricated by Milling technique than that of copings fabricated by DMLS technique.

Mean internal gap value for Subgroup A2 (Milled copings with 65 µm die spacer thickness) was **29.519 µm** with standard deviation of **5.9908 µm** whereas for Subgroup B2 (DMLS copings with 65 µm die spacer thickness) it was found to be **21.264 µm** with standard deviation of **0.8954 µm** (Table 1). These values suggest that there is a statistically highly significant difference with high values in Subgroup A2 as compared to Subgroup B2 suggestive that the internal gap values for metal copings with 65 µm die spacer thickness were higher with copings fabricated by Milling technique than that of copings fabricated by DMLS technique.

Table 2: Inter-Subgroup pairwise comparison of internal gaps (Mann-Whitney U Test)

Subgroup	Vs Subgroup	Mann-Whitney U value	Z value	p value of Mann-Whitney U test
A1	A2	200.000	-1.815	0.070#
B1	B2	112.000	-3.641	0.000**
A1	B1	156.00	-2.725	0.000**
A2	B2	22.000	-5.486	0.000**

Subgroup A1 v/s Subgroup A2 P value was > 0.05 so statistically nonsignificant difference seen. Subgroup B1 v/s Subgroup B2 P value was < 0.01 so statistically highly significant difference seen. Subgroup A1 v/s Subgroup B1 P value was < 0.01 so statistically highly significant difference seen. Subgroup A2 v/s Subgroup B2 P value was < 0.01 so statistically highly significant difference seen (Table 2).

IV. DISCUSSION

Zuskova L et al⁴ in 2019 studied effect of CAD/CAM procedures on the overall fit of metal copings. Die spacer thickness was 55 µm. Milled group displayed a mean offset fit discrepancies of 42.20 µm, while the laser-sintered group showed a mean of 42.24 µm fit discrepancies which was in agreement with the results found in this study. **Vojdani et al¹⁶ in 2016** stated a study that had clinically acceptable results of 23 µm for the internal gap in the CAD/Milling group and 46 µm for the internal gap in the CAD/ Ceramill Sintron. **Bhaskaran et al¹⁷ in 2013** reported internal gap of Co-Cr copings cast from 3D printed resin patterns to be 36.15 µm. Similarly **Park J K et al¹⁹ in 2015** evaluated the Overall mean gap for Co-Cr coping fabricated by the computer-aided milling and DMLS methods were 88.9 µm and 103.3 µm respectively. An explanation of the lack of agreement may be due to difference in measurement approaches and criteria's used while measuring the internal fit and difference in die spacer thickness. Differences in the CAD/CAM fabrication techniques of crown shaved direct influence on their internal fit. **According to Koutsoukis T et al²⁰ in 2015** DMLS performs better than the milling and casting techniques in the primary economic areas, including labor, time, waste of materials and consumables, recycling and productivity. According to **Venkaresh K V et al²¹ in 2013** three main factors affecting the fit are: precision of the scanner, how effectively software can transform the scanning data into a 3D model in the computer and the precision of the milling machine.

In the current study, DMLS technique in comparison with Milled techniques showed lowest internal fit discrepancy for both 40 and 65 µm die spacer thickness. However, within the DMLS technique, 65 µm die spacer thickness showed least internal fit discrepancy followed by 40 µm die spacer thickness. Though the Milling technique, showed a higher internal fit discrepancy for both 40 and 65 µm die spacer thickness, the observed values were within clinically acceptable range. Thereby the results of the study reject the null hypothesis stating that, there exists a significant difference in the internal fit of metal copings with two different die spacer thickness (40 and 65 µm) fabricated by Computer- Aided Milling and Direct Metal Laser Sintering techniques. Thus, the current study was conducted to help the clinician to make a choice among the above mentioned CAD/CAM fabrication techniques and the die spacer thickness for fabrication of Co-Cr copings. Mean Internal gap values observed in Milling technique was statistically nonsignificant whereas, mean internal gap values observed in

DMLS techniques showed statistically significant difference with 40 µm and 65 µm die spacer thickness following an order of B2 < B1.

There were some limitations in this study. Since this is an in-vitro study, it does not directly simulate the intraoral condition. Studies with a larger sample size need to be carried out to obtain more accurate results. The present study was conducted with two different die spacer thickness (40 and 65 µm) but in order to achieve greater accuracy in the results these die spacer thickness (40 and 65 µm) should be further compared in different die spacer thickness.

V. CONCLUSION

Above study provides discrete data and direct comparison on the internal adaptation of Metal copings fabricated by Milling and DMLS techniques with 40 µm and 65 µm die spacer thickness.

The internal fit discrepancies found in this study were within the clinically acceptable standard (120 µm). In the current study DMLS technique in comparison with Milled techniques showed lowest internal fit discrepancy for both 40 and 65 µm die spacer thickness. However, within the DMLS technique, 65 µm die spacer thickness showed least internal fit discrepancy followed by 40 µm die spacer thickness.

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